

Second Supplement to “Frequency Responses of a Neural Oscillator”

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1 The Oscillator with Linear Input

The system dealt with in “Frequency Responses of a Neural Oscillator” is

$$\tau \frac{d}{dt} x_i(t) + x_i(t) = c - ay_j(t) - bv_i(t) - g(\pm u(t)) \quad (i, j = 1, 2; i \neq j), \quad (1)$$

$$T \frac{d}{dt} v_i(t) + v_i(t) = y_i(t) = g(x_i(t)), \quad (2)$$

$$y(t) = y_2(t) - y_1(t). \quad (3)$$

An important feature of this input-output system is in the way of input, $-g(\pm u(t))$. Since $y_j(t)$, $v_i(t)$ and $g(\pm u(t))$ are all non-negative, the right-hand side of (1) never exceeds positive constant c , implying that $x_i(t)$ is bounded to the upper by c . This leads to $0 \leq y_i(t) \leq c$ and hence $-c \leq y(t) \leq c$. Thus we find that the output $y(t)$ of the system is bounded however positively/negatively large the input $u(t)$ is.

If the nonlinear inputs $-g(\pm u(t))$ is replaced by linear inputs $\mp u(t)$ as

$$\tau \frac{d}{dt} x_i(t) + x_i(t) = c - ay_j(t) - bv_i(t) \mp u(t), \quad (4)$$

then the boundedness of the output will be lost. This supplement discusses the frequency response in this case.

2 Describing Function

Carrying out the same calculations as those in “Frequency Responses ...” for the present system, we have

$$\begin{aligned} \tau \frac{d}{dt} \tilde{x}_i(t) + \tilde{x}_i(t) + A_x r_x &= c - a(K(r_x) \tilde{x}_j(t) + A_x L(r_x)) \\ &\quad - b(\tilde{v}_i(t) + A_x L(r_x)) \\ &\quad \mp u(t), \end{aligned} \quad (5)$$

$$T \frac{d}{dt} \tilde{v}_i(t) + \tilde{v}_i(t) = K(r_x) \tilde{x}_i(t), \quad (6)$$

$$y_i = K(r_x) \tilde{x}_i(t) + A_x L(r_x). \quad (7)$$

Defining $x(t) \triangleq \tilde{x}_2(t) - \tilde{x}_1(t)$ and $v(t) \triangleq \tilde{v}_2(t) - \tilde{v}_1(t)$, we obtain a set of linearized equations that relates input $u(t)$ and output $y(t)$:

$$\tau \frac{d}{dt} x(t) + (1 - aK(r_x))x(t) = -bv(t) + 2u(t), \quad (8)$$

$$T \frac{d}{dt} v(t) + v(t) = K(r_x) x(t), \quad (9)$$

$$y(t) = K(r_x) x(t). \quad (10)$$

Applying the Laplace transform to these equations, we obtain the following transfer functions:

$$G(s, A) = \frac{2(Ts + 1)}{\tau Ts^2 + (K_n - K(r_x))Tas + 1 + (\tau T\omega_n^2 - 1) \frac{K(r_x)}{K_n}}, \quad (11)$$

$$N(s, A) = K(r_x) G(s, A). \quad (12)$$

Function $G(s, A)$ represents the transfer function from $u(t)$ to $x(t)$, and function $N(s, A)$ represents that from $u(t)$ to $y(t)$. Substituting s in $G(s, A)$ and $N(s, A)$ by $j\omega$, we have frequency transfer functions or describing functions of the system:

$$G(\omega, A) = \frac{2(jT\omega + 1)}{1 + (\tau T\omega_n^2 - 1) \frac{K(r_x)}{K_n} - \tau T\omega^2 + j(K_n - K(r_x))T\omega}, \quad (13)$$

$$N(\omega, A) = K(r_x) G(\omega, A). \quad (14)$$

In the same way as ‘‘Frequency Response ...’’ the following holds:

$$A_x = \frac{1}{2} |G(\omega, A)| A. \quad (15)$$

The obtained describing functions do not look so different from those of the previous model; the only difference is that 2 in the numerator of (13) is missing in the previous model. Actually, however, $r_x = r_x(\omega, A)$ is different between them. Extracting the bias components from (5), we have $A_x r_x = c - aA_x L(r_x) - bA_x L(r_x)$ or

$$A_x \{r_x + (a + b)L(r_x)\} = c. \quad (16)$$

Combining (15) and (16), we obtain $\{r_x + (a + b)L(r_x)\} |G(\omega, A)| = \frac{2c}{A}$ or

$$\frac{\{r_x + (a+b)L(r_x)\} |jT\omega + 1|}{|1 + (\tau T\omega_n^2 - 1) \frac{K(r_x)}{K_n} - \tau T\omega^2 + j(K_n - K(r_x))Ta\omega|} = \frac{c}{A}. \quad (17)$$

This equation implicitly defines function $r_x = r_x(\omega, A)$. In the previous model the right-hand side of the corresponding equation was $2\left(\frac{c}{A} - \frac{1}{\pi}\right)$.

3 Dependency of the Frequency Response on the Input Amplitude

If the amplitude of the sinusoidal input is small, the output will be a mixture of an oscillator-originated wave and an input-originated one. As the amplitude increases and exceeds a critical value, the so-called entrainment occurs; the inherent oscillation originated from the oscillator completely disappears. Transfer function $G(s, A)$ was derived based on the assumption that the oscillator entrains to the sinusoidal input. However, when the input amplitude is too small and hence $K(r_x)$ is large, $G(s, A)$ enters an unstable region. The critical amplitude below which the system becomes unstable can be considered the lower bound of the entrainment.

Equation (11) implies that the stable-unstable transition occurs when

$$K(r_x) = K_n \left(= \frac{\tau + T}{Ta} \right). \quad (18)$$

In this situation, (12) with (11) becomes

$$N(s, A) = \frac{2K_n(Ts + 1)}{\tau T(s^2 + \omega_n^2)}. \quad (19)$$

The linear system theory tell us that, without input, this system generates a periodic oscillation of frequency ω_n , which is the inherent frequency of the oscillator. Thus, it can be predicted that the complete entrainment occurs when $K(r_x) < K_n$.

Substituting $K(r_x) = K_n$ or $r_x = K^{-1}(K_n)$ into (17) and solving it with respect to A , we find the minimum amplitude of the input for entrainment. We denote it by $A_0(\omega)$:

$$A_0(\omega) = \frac{\tau T |\omega^2 - \omega_n^2|}{\sqrt{T^2\omega^2 + 1}} A_n, \quad (20)$$

where

$$A_n \triangleq \frac{c}{K^{-1}(K_n) + (a+b)L(K^{-1}(K_n))}. \quad (21)$$

In the previous model the minimum amplitude for entrainment was

$$A_0(\omega) = \frac{c}{\frac{1}{2} \frac{\sqrt{T^2\omega^2 + 1}}{\tau T |\omega^2 - \omega_n^2|} \frac{c}{A_n} + \frac{1}{\pi}}. \quad (22)$$

There is a big difference between (20) and (22). Function (20) is an unbounded function with respect to ω ; $A_0(\omega) \rightarrow \infty$ for $\omega \rightarrow \infty$. In contrast, function (22) is bounded; $A_0(\omega) < \pi c$.

Next let us investigate what will happen when the input amplitude is very large. For $A \rightarrow \infty$, (17) reduces to

$$r_x + (a + b)L(r_x) = 0.$$

Thus, we find that the present system with $A \rightarrow c$ has essentially the same frequency response as that of the previous system with $A = \pi c$; see “A supplement to ‘Frequency Responses of a Neural Oscillator’”. In the previous system, as the input amplitude increases further than πc and reach a certain finite value $A_1(\omega)$, the output totally vanishes, i.e., $N(\omega, A_1(\omega)) = 0$. Such a phenomenon does not occur in the present system.